

## Enhanced piezoelectricity in Na and Ce co-doped $\text{CaBi}_4\text{Ti}_4\text{O}_{15}$ ceramics for high-temperature applications

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**Abstract:** The sodium (Na) and Ce co-doped calcium bismuth titanate (CBT;  $\text{CaBi}_4\text{Ti}_4\text{O}_{15}$ ) Aurivillius ceramics in a  $\text{Ca}_{1-x}(\text{Na}_{0.5}\text{Ce}_{0.5})_x\text{Bi}_4\text{Ti}_4\text{O}_{15}$  (CNCBT; doping content ( $x$ ) = 0, 0.03, 0.05, 0.08 and 0.12) system were synthesized by the conventional solid-state sintering method. All compositions show a single-phase orthorhombic (space group:  $A2_1am$ ) structure at room temperature. The shift of the Curie point ( $T_C$ ) towards lower temperatures ( $T$ ) on doping results from the increased tolerance factor ( $t$ ). The substitution-enhanced ferroelectric performance with large maximum polarization ( $P_m$ ) and facilitated domain switching is evidenced by the developed electrical polarization–electric field ( $P$ – $E$ ) and electrical current–electric field ( $I$ – $E$ ) hysteresis loops. The piezoelectric coefficient ( $d_{33} = 20.5 \pm 0.1$  pC/N) of the  $x = 0.12$  sample is about four times larger than that of pure CBT. The improved piezoelectric properties can be attributed to the high remanent polarization ( $P_r$ ) and relatively high dielectric permittivity ( $\epsilon'$ ). In addition, multi-sized (micron and sub-micron) domain structures were observed in the CNCBT ceramics by the piezoresponse force microscope (PFM). The multiple-sized ferroelectric domain structure with smaller domains is beneficial to the easy domain switching, enhanced ferroelectric performance, and improved piezoelectric properties of the CNCBT ceramics. The designed Aurivillius-phase ferroelectric ceramics with the  $T_C$  around 765 °C and high piezoelectric coefficient ( $d_{33}$ ) are suitable for high-temperature piezoelectric applications.

**Keywords:** Aurivillius-phase ceramics; high Curie point; domain switching; piezoelectric properties

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## 1 Introduction

Bismuth layer-structured ferroelectrics (BLSFs) belong to a family of Aurivillius-phase materials characterized by a general formula of  $(\text{Bi}_2\text{O}_2)^{2+}(\text{A}_{m-1}\text{B}_m\text{O}_{3m+1})^{2-}$  (where A is a divalent ion or a combination of alkali and lanthanides occupying the dodecahedral coordination site, B is usually a transition metal ion occupying the octahedral coordination site, and  $m$  is the number of  $\text{BO}_6$  octahedra in the  $(\text{A}_{m-1}\text{B}_m\text{O}_{3m+1})^{2-}$  perovskite layer separated by two  $(\text{Bi}_2\text{O}_2)^{2+}$  layers [1]). The  $m$  can be an integer number or a rational number (1.5, 2, 2.5, 3, etc.) typically not bigger than 5 to ensure good dielectric, ferroelectric, and piezoelectric properties of BLSFs. Calcium bismuth titanate (CBT;  $\text{CaBi}_4\text{Ti}_4\text{O}_{15}$ ), as a member of the  $m = 4$  family of BLSFs, is a potential candidate for high-temperature piezoelectric and ferroelectric applications such as sensors, filters, or oscillators because of its high Curie point ( $T_C \approx 790^\circ\text{C}$ ), good thermal stability, low aging, and low dielectric loss tangent ( $\tan\delta$ ) [2,3]. However, a commercial application of CBT ceramics is limited due to their weak piezoelectricity (piezoelectric coefficient ( $d_{33}$ )  $< 5$  pC/N). The relatively low values of  $d_{33}$  are related to a high coercive field ( $E_c$ ) of CBT, which makes it difficult to switch ferroelectric domains by direct current (DC) or alternating current (AC) poling.

Numerous experimental techniques and methods have been developed to improve the piezoelectric properties of CBT. It was demonstrated that the spark plasma sintering [4], cold-pressing [5], and ion engineering methods [6–8] can effectively improve the piezoelectric and ferroelectric performances of BLSFs. Among these approaches, ion doping appears to be the most viable method for industrial fabrication as it enables to easily modify the sintering activity, microstructure, and electrical properties at low costs. It has been reported that a partial substitution of CBT at A sites with lanthanides, e.g., La, can greatly improve its piezoelectric properties [8]. The  $d_{33}$  of La-doped CBT was about 11 pC/N, and the high piezoelectricity was explained by the increased Bi : Ca ratio [8]. However, the  $T_C$  decreases on La doping, which hinders the use of this material at high temperatures ( $T$ ). An enhancement of the  $d_{33}$  ( $\sim 15$  pC/N) and a small shift of  $T_C$  towards higher temperatures were observed in vanadium (V)-doped CBT ceramics [9]. The V-doping effects were explained by the higher valence of  $\text{V}^{5+}$  ions, if

compared to the valence of  $\text{Ti}^{4+}$  ions, introducing the cation vacancy, which may improve the structure distortion, and thus increase  $T_C$  [9,10]. Aside from the single doping, equally co-doped CBT ceramics at the A site with lanthanides (e.g.,  $\text{Er}^{3+}$ ,  $\text{Nd}^{3+}$ ,  $\text{Ho}^{3+}$ , and  $\text{Ce}^{3+}$ ) and alkaline metals (e.g.,  $\text{Na}^+$ ,  $\text{Li}^+$ , and  $\text{K}^+$ ) have been recently proposed for the investigation of improved ferroelectric and piezoelectric properties [11–15]. In Ref. [12], it has been found that  $\text{Ca}_{1-x}(\text{A,Ce})_{x/2}\text{Bi}_4\text{Ti}_4\text{O}_{15}$  ( $x$  is the doping content, and  $\text{A} = \text{Li}$ ,  $\text{Na}$ , and  $\text{K}$ ) ceramics exhibit high electrical resistivity and  $d_{33}$  at high temperatures compared to pure  $\text{CaBi}_4\text{Ti}_4\text{O}_{15}$  ceramics. However, neither the ferroelectric behaviour nor the domain morphology of the doped ceramics was investigated thoroughly. A comprehensive understanding of the effect of the double doping with alkaline and rare-earth ions on the crystal structure, domain structure, dielectric, piezoelectric, and ferroelectric properties of CBT is still missing.

In the present study, Na was chosen for co-doping of the above  $\text{Ca}_{1-x}(\text{A,Ce})_{x/2}\text{Bi}_4\text{Ti}_4\text{O}_{15}$  system, because  $\text{Li}^+$  is known easily evaporated during sintering at high temperatures, and  $\text{K}^+$  can dramatically lower the  $T_C$  due to its large radius [12]. The designed  $\text{Ca}_{1-x}(\text{Na}_{0.5}\text{Ce}_{0.5})_x\text{Bi}_4\text{Ti}_4\text{O}_{15}$  (CNCBT;  $x = 0, 0.03, 0.05, 0.08,$  and  $0.12$ ) ceramic system is investigated for the underlying mechanisms between crystal structures, domain morphologies, and electrical properties. Moreover, the domain engineering approach is adapted in the preparation of the Na and Ce co-doped samples to obtain a multiple domain structure with a reduced  $E_c$ , large maximum polarization ( $P_m$ ), and relatively high dielectric permittivity ( $\epsilon'$ ). The lower  $E_c$  and larger  $\epsilon'$  are crucial to enhancing the  $d_{33}$  as well as the electromechanical coupling factors in Aurivillius CBT-based ceramics. Thus, the proposed approach provides a guide for future material design and performance optimization of Aurivillius-phase ceramics in high-temperature piezoelectric sensors and actuators.

## 2 Materials and methods

The  $\text{Ca}_{1-x}(\text{Na}_{0.5}\text{Ce}_{0.5})_x\text{Bi}_4\text{Ti}_4\text{O}_{15}$  ceramics with  $x = 0, 0.03, 0.05, 0.08,$  and  $0.12$  (abbreviated hereafter as CBT, CNCBT3, CNCBT5, CNCBT8, and CNCBT12, respectively) were synthesized via the traditional solid-state reaction method. The starting materials were powders of  $\text{CaCO}_3$  (Alfa Aesar, purity  $> 99.8\%$ ),

NaCO<sub>3</sub> (Alfa Aesar, purity = 99.8%), CeO<sub>2</sub> (Sigma Aldrich, purity = 99.9%), TiO<sub>2</sub> (Sigma Aldrich, purity = 99.8%), and Bi<sub>2</sub>O<sub>3</sub> (Sigma Aldrich, purity = 99.9%). After pre-heating at 200 °C for 24 h, these chemicals were weighed according to the stoichiometric composition. The mixture was ground in ethanol for 6 h with Y-stabilized ZrO<sub>2</sub> balls in nylon bottles using a planetary ball mill (Planetary Mill PULVERISETTE 5/4, FRITSCH, German). The slurry was dried at 100 °C overnight. The dried powders were calcined at 800 °C, and then at 900 °C for 2 h in a programmable furnace (30-3000 C, Nabertherm, UK). The calcined powders were ball-milled again for 6 h to reduce the particle size. Then, 5 wt% polyvinyl alcohol (PVA) was added into the calcined powders, and the mixture was pressed into disks (13 mm in diameter and 1–2 mm in thickness) at a pressure of 100 MPa. The pellets were heated at 800 °C for 2 h without the lid to remove the PVA binder. After that, the pellets were inserted into an alumina crucible, covered by the coarse ZrO<sub>2</sub> powders and sintered at 1150 °C for 2 h in the air.

The crystal structures of the sintered CBT-derived ceramics were investigated on crushed powders over the  $2\theta$  range from 5° to 120° using an X-ray diffractometer (Cubix, PANalytical, the Netherlands) with Ni-filtered Cu K $\alpha$  radiation ( $\lambda = 1.5418 \text{ \AA}$ ). The Rietveld refinement analysis of the X-ray diffraction (XRD) data within a wide range was performed by means of the General Structure Analysis System (GSAS) software [16] combined with the EXPGUI interface [17]. The microstructures of the thermally etched ceramics (the well-polished ceramics were annealed at a temperature typically 100 °C below the sintering temperature for 2 h) [18,19] were observed using a scanning electron microscope (SEM; FEI Inspect-F, USA). The grains are plate-like with similar thicknesses. The average grain size (perpendicular to the thickness direction) is derived from the average grain length within the scanning area, which was measured and calculated via the Image J software. The ferroelectric domain structure was studied on the unpoled samples after well mirror polishing without annealing by the piezoresponse force microscope (PFM, Bruker, USA) both in the vertical and lateral modes. The scanning area is 5  $\mu\text{m} \times 5 \mu\text{m}$ , and the drive amplitude of the electric field ( $E$ ) is 10 V. The surface element analysis of ceramics was performed with an X-ray photoelectron spectrometer (Nexsa XPS system, Thermo Fisher Scientific, USA). The X-ray

photoelectron spectroscopy (XPS) spectra were fitted by the Gaussian–Lorentzian product function implemented in the commercial Advantage software [20]. For the dielectric, ferroelectric, and piezoelectric measurements, the as-sintered ceramics were electroded on major surfaces by a platinum paste (C2011004D5, Gwent Electronic Materials Ltd., UK). The temperature dependence of the relative  $\epsilon'$  and  $\tan\delta$  was measured in the temperature range of 25–900 °C with a heating rate of 3 °C/min at various frequencies from 1 kHz to 1 MHz with an LCR meter (4284A, Agilent, USA) connected to a tube furnace. Both the electrical polarization–electric field ( $P$ – $E$ ) and electrical current–electric field ( $I$ – $E$ ) loops were measured in silicon oil at room temperature (RT) using a ferroelectric tester (NPL made with a pair of NXB2-AL nanosensors, HP33120A function generator and LabView software controlled, Teddington, UK) [21]. The testing frequency of the triangular voltage waveforms was set to 10 Hz. The samples were poled in silicone oil under a DC field of 8 kV/mm at 150 °C for 10–15 min, and then depoled at selected temperatures for 2 h from RT to 700 °C. The  $d_{33}$  was measured with a  $d_{33}$  meter (ZJ-3AN, Institute of Acoustics Academia, Beijing, China). The planar and thickness electromechanical coupling factors ( $K_p$  and  $K_t$ ) and the mechanical coupling factor ( $Q_m$ ) were determined by the resonance–antiresonance method [22,23] using the data collected by an LCR meter (4284A, Agilent, USA).

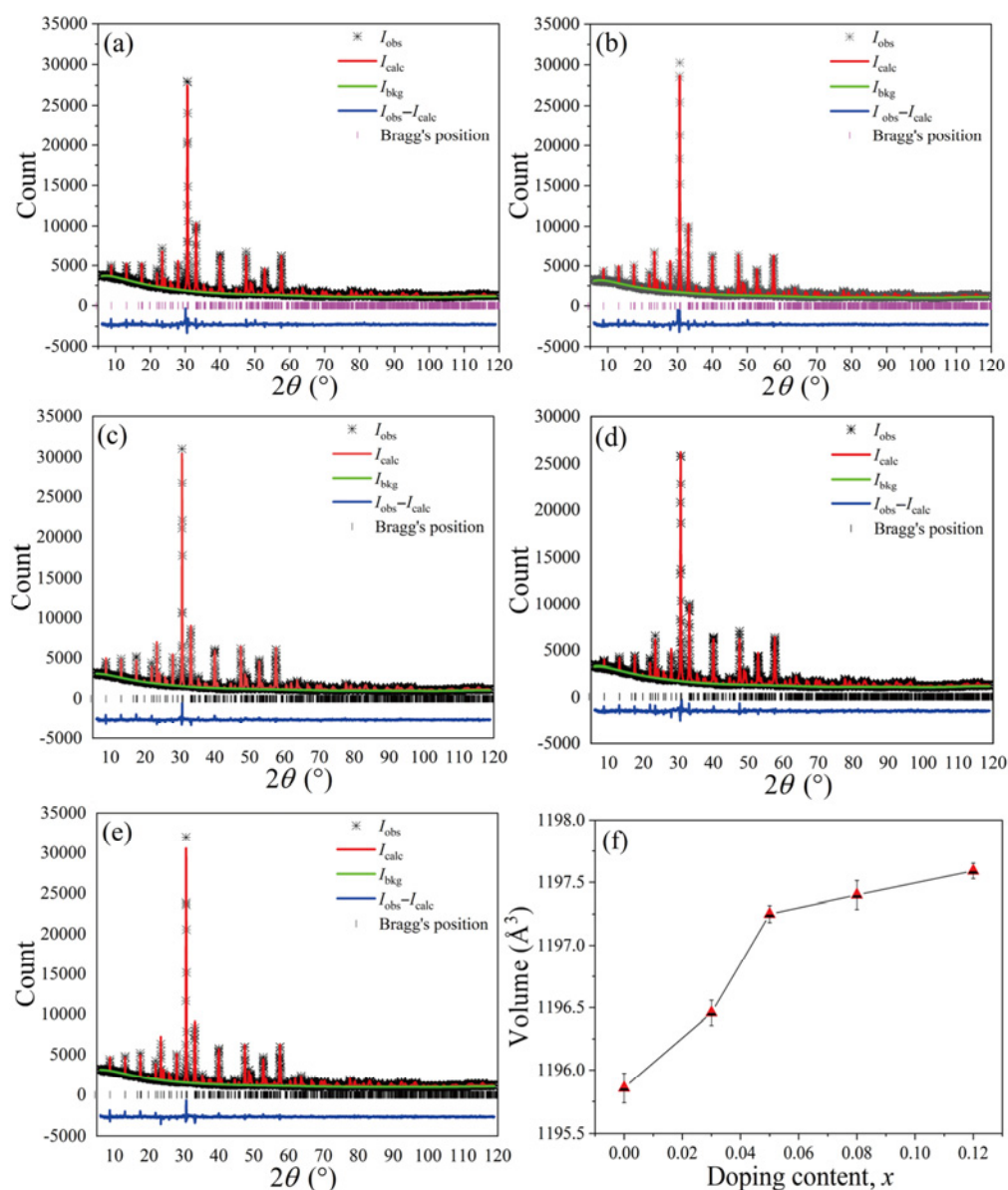
### 3 Results and discussion

The measured relative densities are 96.1%, 96.1%, 96.2%, 96.2%, and 96.1% for Ca<sub>1-x</sub>(Na<sub>0.5</sub>Ce<sub>0.5</sub>)<sub>x</sub>Bi<sub>4</sub>Ti<sub>4</sub>O<sub>15</sub> ( $x = 0, 0.03, 0.05, 0.08, \text{ and } 0.12$ ) ceramics, respectively. Figure S1 in the Electronic Supplementary Material (ESM) shows the XRD patterns of the Ca<sub>1-x</sub>(Na<sub>0.5</sub>Ce<sub>0.5</sub>)<sub>x</sub>Bi<sub>4</sub>Ti<sub>4</sub>O<sub>15</sub> ( $x = 0, 0.03, 0.05, 0.08 \text{ and } 0.12$ ) ceramics at RT. The labelled  $hkl$  indices correspond to those of the reference orthorhombic-structured CBT samples with the  $A2_1am$  symmetry (PDF#52-1640). The Na and Ce co-doped CBT ceramics show almost the same diffraction reflections as pure CBT without any traces of a secondary phase. Hence, the Na and Ce ions are assumed to enter the lattice and form the  $m = 4$  Aurivillius phase at RT. The Rietveld structure refinements of the XRD data were

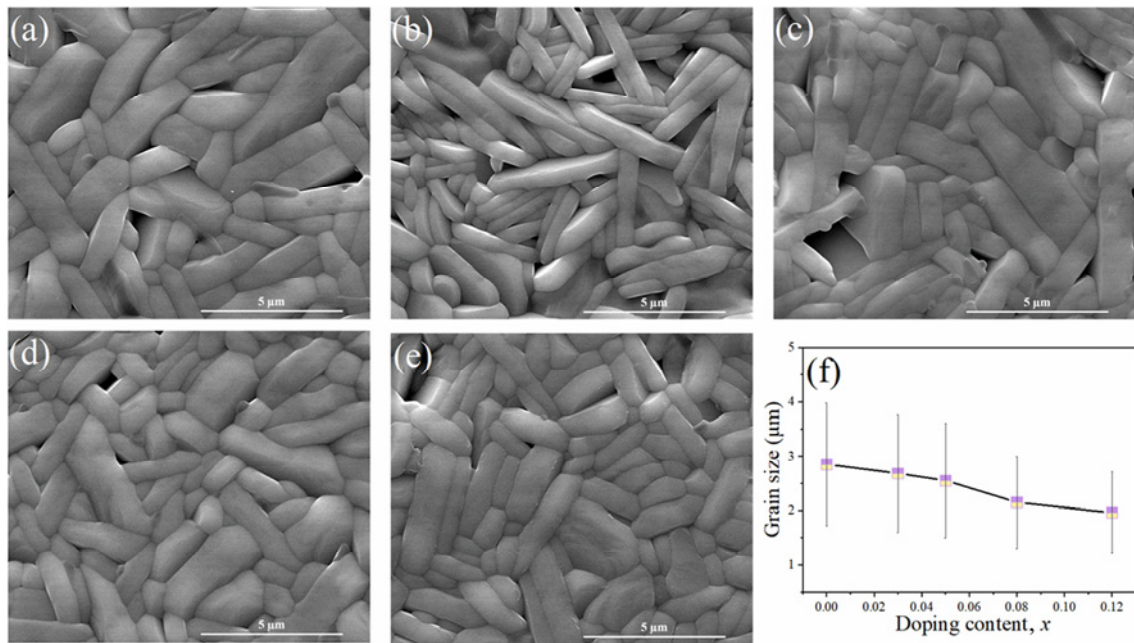
carried out to further investigate the structural changes induced by the Na and Ce doping (Fig. 1). The refinement details as well as the refined structure parameters are given in Table S1 in the ESM. The lattice expansion, as shown in Fig. 1(f), can be probably attributed to the bigger average ionic radii of  $\text{Na}^+$  (1.39 Å) and  $\text{Ce}^{3+}$  (1.34 Å) ions, if compared to that of  $\text{Ca}^{2+}$  (1.34 Å) [24]. Few  $\text{Ce}^{4+}$  ions (less than half of  $\text{Ce}^{3+}$  ions) with a smaller radius (1.14 Å) also existed here supporting by the later XPS analysis, which is not the dominant reason for the volume change.

The microstructure images of the CNCBT ceramics

are shown in Fig. 2. Dense CNCBT ceramic samples were obtained by the optimized sintering process, confirming the calculated density of the sintered samples by the Archimedes method. The observation of anisotropic plate-like shaped grains is in accordance with the data previously reported on single-phase Aurivillius ceramics [15]. The average grain sizes decrease slightly on doping from  $2.85 \pm 1.13 \mu\text{m}$  (CBT) to  $2.68 \pm 1.08 \mu\text{m}$  (CNCBT3),  $2.55 \pm 1.05 \mu\text{m}$  (CNCBT5),  $2.15 \pm 0.85 \mu\text{m}$  (CNCBT8), and  $1.96 \pm 0.75 \mu\text{m}$  (CNCBT12) (Fig. 2(f)), which can be possibly explained by the co-doping of Na and Ce ions with different radii compared with  $\text{Ca}^{2+}$ . Co-dopants with



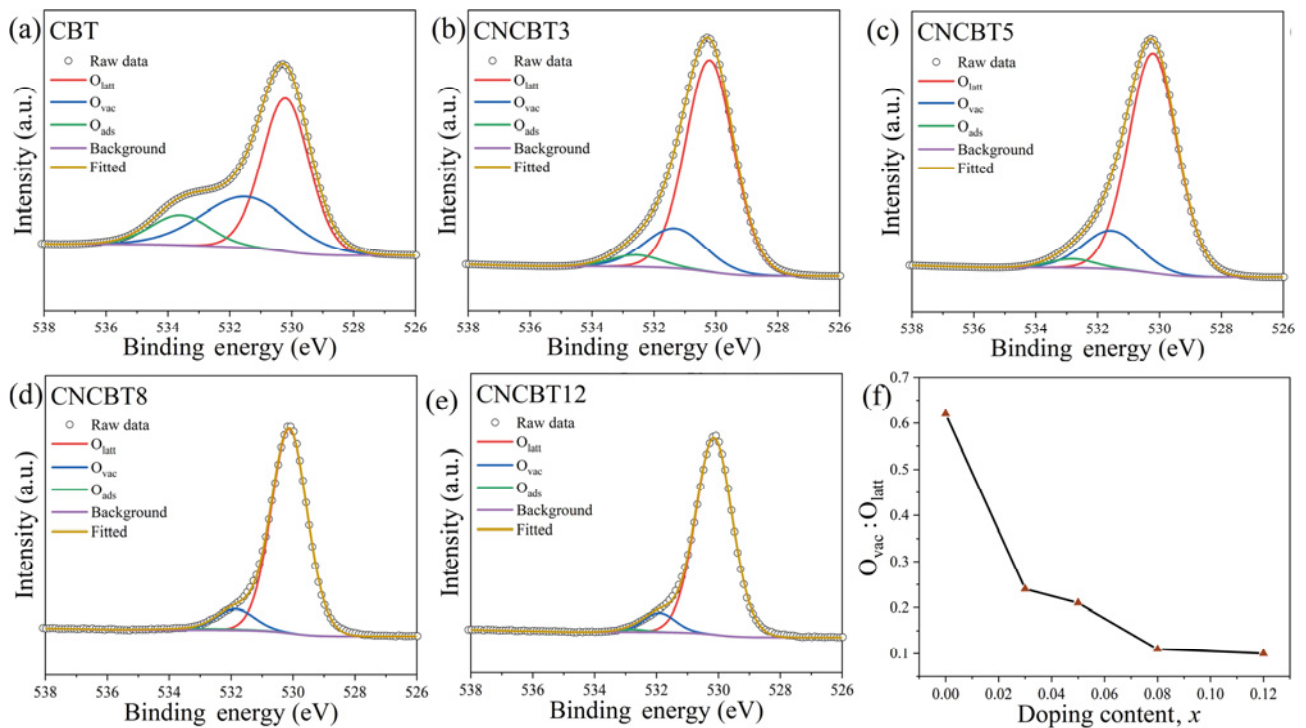
**Fig. 1** Rietveld refinements of the XRD patterns for (a) CBT, (b) CNCBT3, (c) CNCBT5, (d) CNCBT8, and (e) CNCBT12 ceramics. (f) Compositional dependence of unit cell volume ( $I_{\text{obs}}$ : measured pattern,  $I_{\text{calc}}$ : calculated pattern, and  $I_{\text{obs}} - I_{\text{calc}}$ : difference).



**Fig. 2** Micrographs of (a) CBT, (b) CNCBT3, (c) CNCBT5, (d) CNCBT8, and (e) CNCBT12 ceramics (after thermal etching). (f) Compositional dependence of grain size.

different radii can produce the local stress field at the lattice level, which is the barrier for the diffusion of ions. Hence, the grain size decreases with the increasing  $x$ , which can be attributed to the lower diffusivity caused by the local stress field [25].

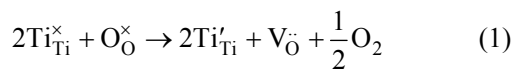
To explore the chemical states of oxygen and check for an existence of oxygen vacancies ( $O_{vac}$ ), the surface elemental analysis on CNCBT ceramics was carried out by the XPS. The fitted O 1s XPS spectra are shown in Fig. 3. The deconvolution of the O 1s spectral peak



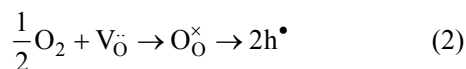
**Fig. 3** Fitted XPS spectra of O 1s peaks for (a) CBT, (b) CNCBT3, (c) CNCBT5, (d) CNCBT8, and (e) CNCBT12 ceramics. (f) Compositional dependence of  $O_{vac} : O_{latt}$  ratio.

gives three overlapping peaks—The first peak lattice oxygen ( $O_{\text{latt}}$ ) at a lower binding energy (~530 eV) is associated with the intrinsic state of O (the red line), the second peak  $O_{\text{vac}}$  at a moderate binding energy (~531 eV) corresponds to the oxygen in the deficient region (the blue line), and the third peak of the adsorbed oxygen ( $O_{\text{ads}}$ ) at a higher binding energy (~533 eV) can be linked with  $O_{\text{ads}}$  from the air (the green line) [26,27]. The ratio of  $O_{\text{vac}} : O_{\text{latt}}$  corresponds to the concentration of oxygen vacancies in the prepared compositions [28]. The binding energies for three peaks and the  $O_{\text{vac}} : O_{\text{latt}}$  ratio are listed in Table S2 in the ESM. The estimated  $O_{\text{vac}} : O_{\text{latt}}$  values decrease from 0.62 to 0.24, 0.21, 0.12, and 0.10 for the samples of CBT, CNCBT3, CNCBT5, CNCBT8, and CNCBT12, respectively.

The existence of oxygen vacancies can be possibly due to the reduction of  $\text{Ti}^{4+}$  cations during the sintering, which is common in piezoelectric ceramics prepared by the solid-state sintering method. The underlying mechanism can be described by the Kröger–Vink notation, as reported in other perovskite ferroelectric ceramics [29].



The holes were then generated because samples adsorb ambient oxygen on the specimen surface during cooling based on Reaction (2):



The fitted Ti 2p XPS spectra including six well de-convoluted peaks, as presented in Fig. S2 in the ESM, clearly demonstrate the existence of  $\text{Ti}^{3+}$  and  $\text{Ti}^{4+}$  for all CNCBT ceramics [29,30]. All binding energies and  $\text{Ti}^{3+} : \text{Ti}^{4+}$  ratios deduced from Fig. S2 are listed in Table S3 in the ESM. The decreasing trend of  $\text{Ti}^{3+} : \text{Ti}^{4+}$  is consistent with that of the oxygen vacancies. In addition, the high-resolution Ce XPS spectra well fitted by eight typical peaks support the co-existence of  $\text{Ce}^{3+}$  and  $\text{Ce}^{4+}$  cations [31], as presented in Fig. S3 in the ESM. All binding energies and semi-quantified  $\text{Ce}^{3+} : \text{Ce}^{4+}$  ratios deduced from Fig. S3 in the ESM are listed in Table S4 in the ESM. The Ce as the donor dopant can provide extra electrons to reduce the concentration of holes, which can be expressed by Reactions (3)–(5) [32]:

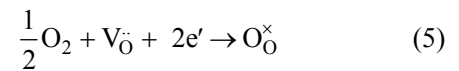
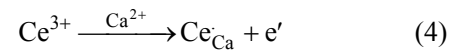
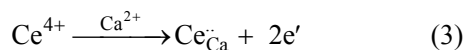


Figure 4 displays the plots of  $\epsilon'$  and  $\tan\delta$  as a function of  $T$  for the CNCBT ceramics. All compositions show a sharp  $\epsilon'(T)$  peak near 800 °C, indicating a narrow ferroelectric to paraelectric phase transition. The  $T_{\text{C}}$  for CBT, CNCBT3, CNCBT5, CNCBT8, and CNCBT12 are 784±1, 783±1, 781±1, 770±1, and 765±1 °C, respectively (at 500 kHz). These values match well with the previously reported Aurivillius materials [33]. The substitution-induced decrease of  $T_{\text{C}}$  can be ascribed to the changes of tolerance factor ( $t$ ).

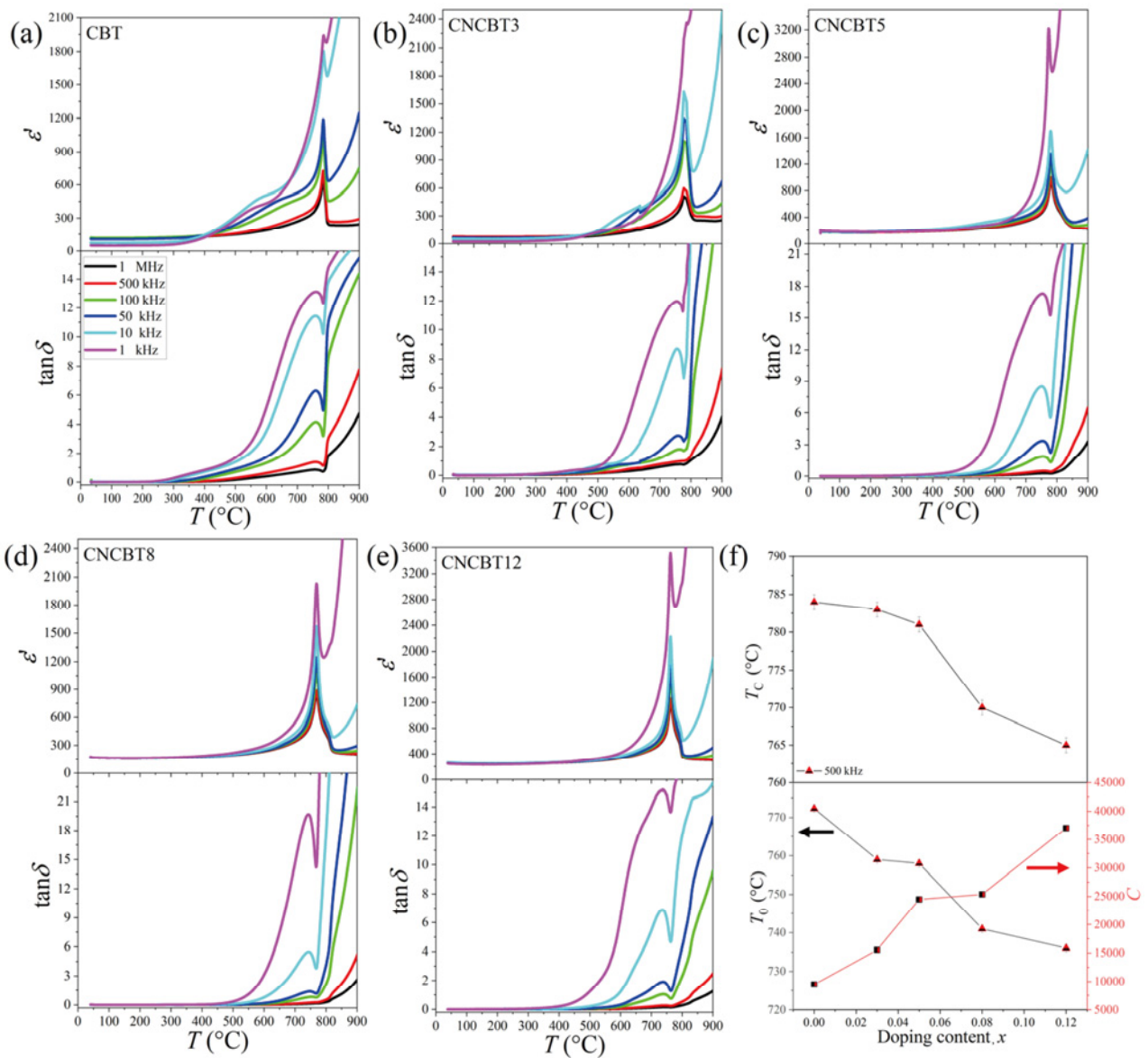
$$t = (R_{\text{A}} + R_{\text{O}}) / [\sqrt{2}(R_{\text{B}} + R_{\text{O}})] \quad (6)$$

where  $R_{\text{A}}$ ,  $R_{\text{O}}$ , and  $R_{\text{B}}$  are the effective average radii of divalent ions, oxygen, and ions at the octahedral sites, respectively. In general,  $T_{\text{C}}$  decreases when  $t$  increases due to the structure distortion [10]. Upon  $\text{Na}^+$  and  $\text{Ce}^{3+/4+}$  co-doping, the  $t$  increases from 0.9730 to 0.9733, 0.9735, 0.9739, and 0.9742 for CBT, CNCBT3, CNCBT5, CNCBT8, and CNCBT12 ceramics, respectively, which is consistent with the reduction of  $T_{\text{C}}$ .

With the increasing amount of Na and Ce ions, the frequency dependence of permittivity especially at high frequencies is weakened. Specifically, the enhanced dielectric dispersion ( $\epsilon'_{\text{m}}(100 \text{ kHz}) - \epsilon'_{\text{m}}(1 \text{ kHz})$ ) decreases from 595 to 415, 280, 185, and 160 for the CBT, CNCBT3, CNCBT5, CNCBT8, and CNCBT12 ceramics, respectively, which can be attributed to the reduction of oxygen vacancies. Above  $T_{\text{C}}$ , the permittivity drops greatly, but then it increases again due to the space-charge effects activated by the thermal energy, as reported for BNT-based dielectrics [34]. For temperatures between  $T_{\text{C}}$  and 810 °C, the Curie–Weiss (C–W) behaviour of the permittivity was investigated by Eq. (7) [35]:

$$\frac{1}{\epsilon'} = \frac{T - T_0}{C} \quad (7)$$

Figure 4(f) shows plots of  $T_0$ ,  $T_{\text{C}}$ , and  $C$  (obtained from the C–W fits at 500 kHz) of the CNCBT ceramics against  $x$ . The difference between  $T_0$  and  $T_{\text{C}}$  indicates the first-order phase transition in all samples. Both  $T_0$  and  $T_{\text{C}}$  decrease with the substitution-driven increase of the  $t$ , as discussed above. The calculated  $C$  is in the magnitude of  $10^4$  for all the compositions and matches well with the value reported for other dielectrics with a perovskite structure [36].



**Fig. 4** Temperature dependence of  $\epsilon'$  and  $\tan\delta$  at six selected frequencies for (a) CBT, (b) CNCBT3, (c) CNCBT5, (d) CNCBT8, and (e) CNCBT12 ceramics. (f)  $T_c$ , C–W temperature ( $T_0$ ), and C–W constant ( $C$ ) against  $x$ .

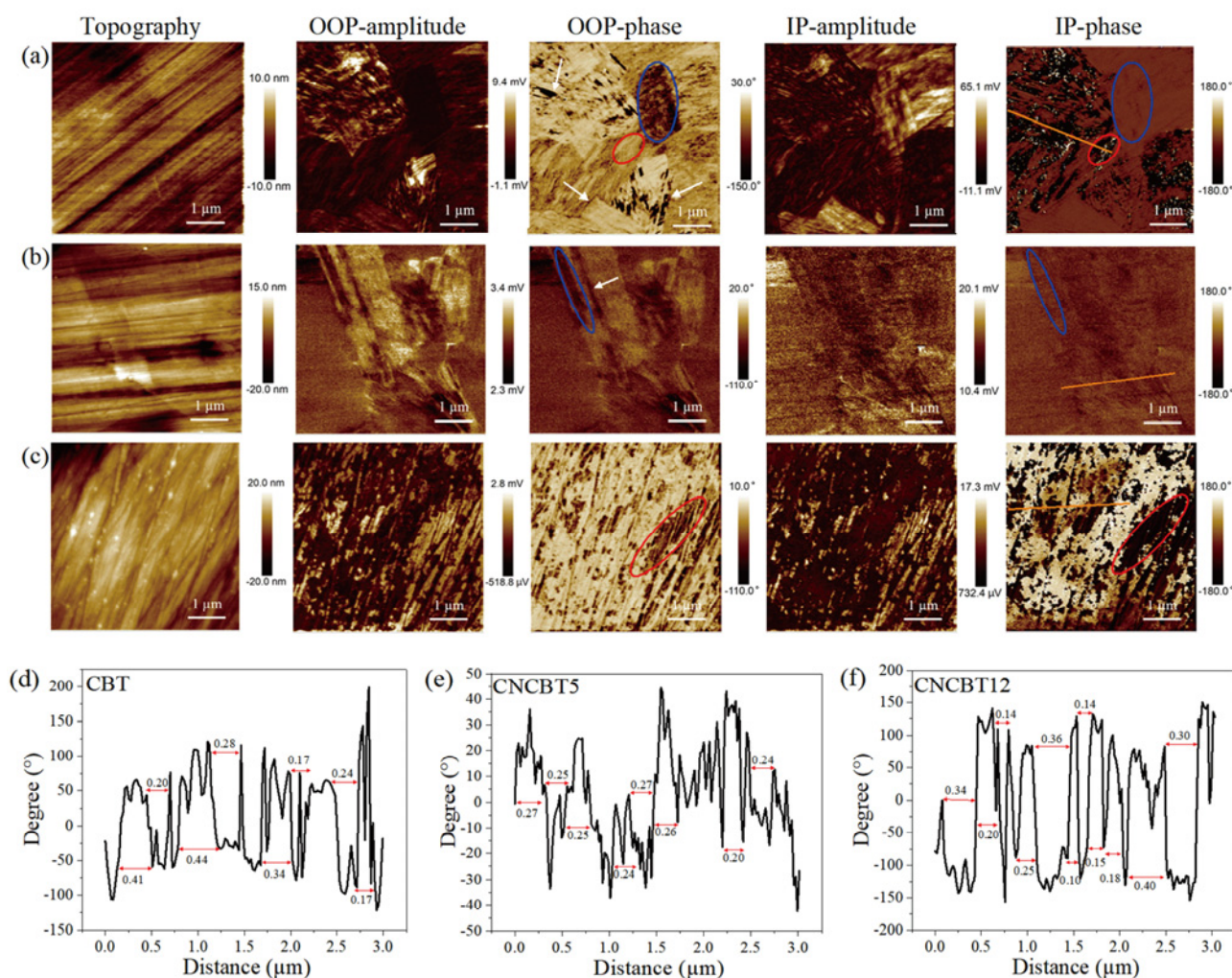
The loss is related to the AC conductivity and frequency-independent DC conductivity [37]. In Fig. 4, high losses at low frequencies can be attributed to contributions both from the friction of dipoles and DC conductivity. At high frequencies, the contribution of the friction of dipoles is dramatically decreased because many dipoles cannot follow the applied AC field, which indicates that the loss measured at high frequencies is dominated by DC conductivity. In Fig. 4, the loss measured at 1 MHz below 500 °C decreases with the increasing  $x$ , which suggests that the developed ceramics show high resistivity below 500 °C. Obviously, the  $\tan\delta$  exhibit a peak below  $T_C$  (at about

750 °C) due to the enhanced viscous movement of ferroelectric domain walls near the  $T_C$ . Additionally, an anomaly (a small broad peak) is observed in CBT and CNCBT3 around 600 °C and can be attributed to the thermally activated oxygen ion jump mechanism proposed in Ref. [38].

The representative topography and out-of-plane (OOP) and in-plane (IP) PFM amplitude and phase images of the  $\text{Ca}_{1-x}(\text{Na}_{0.5}\text{Ce}_{0.5})_x\text{Bi}_4\text{Ti}_4\text{O}_{15}$  ( $x = 0, 0.05$  and  $0.12$ ) ceramics within a selected area of  $5 \mu\text{m} \times 5 \mu\text{m}$  are shown in Figs. 5(a)–5(c). The complex ferroelectric domain structure with micron/sub-micron sized domains and different polarization orientations is evidenced by

the distinguishable phase contrast between the bright areas or dots and the brown regions [39]. The roughness for scanned ceramics is pretty low (within 20 nm) though some scratches can be seen in the topography images, which do not affect the amplitude and phase images greatly because scratches are not overlapped with domain walls. It is obvious that the piezoelectric response in the lateral plane is higher than that of the vertical PFM images supported by the absolute piezoresponse in the amplitude images and the large phase contrast in the phase images, which can be explained by the polarization vector for CNCBT ceramics along the  $a$ -axis, i.e., perpendicular to the thickness plane of plate-like grains [40]. Usually, grains of Aurivillius phase ceramics with an even number of  $m$  prefer thickness-plane oriented, which do not contribute to a vertical PFM response because there is no polarization along  $c$ -axis according to their

space group  $A2_1am$ , as shown by the domains indicated by the red circles. However, some domains (indicated by the blue circles in the PFM phase images) show high response in the vertical mode and weak response in the lateral mode, suggesting that lateral-plane oriented grains exist in the non-textured ceramics. Overall, both thickness-plane oriented and lateral-plane oriented grains exist in the prepared CNCBT ceramics. Strip-like domains, as denoted by the white arrows in Figs. 5(a) and 5(b), represent non-180° domains, which are 90° domain walls in orthorhombic-structured piezoelectric ceramics [41,42]. Moreover, smaller domains with nanometer sizes were observed in highly doped CNCBT ceramics like CNCBT12, and the average domain sizes are 0.28, 0.25, and 0.23  $\mu\text{m}$  for CBT, CNCBT5, and CNCBT12 samples, respectively, calculated from the PFM line profile analysis [43], as shown in Figs. 5(d)–5(f). As shown in Fig. 2(f), the



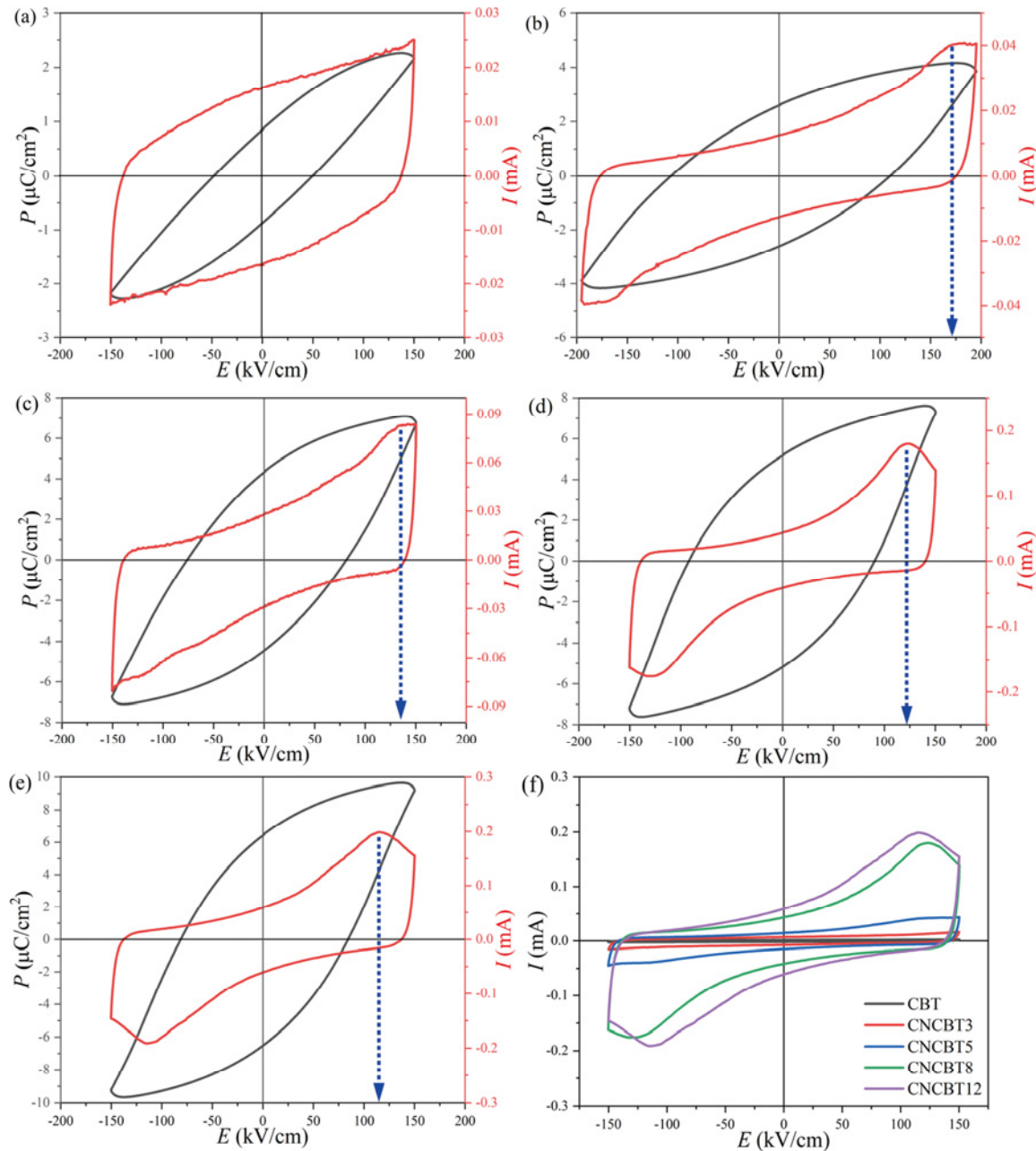
**Fig. 5** (a–c) Topography and OOP and IP PFM amplitude and phase images of polished  $\text{Ca}_{1-x}(\text{Na}_{0.5}\text{Ce}_{0.5})_x\text{Bi}_4\text{Ti}_4\text{O}_{15}$  ( $x = 0, 0.05, \text{ and } 0.12$ ) ceramics. (d–f) Corresponding line profile analyses deduced from the orange lines in the IP phase images.



grain size decreases with the increasing  $x$ . In this case, small domains are favoured in highly doped CNCBT ceramics with a high grain boundary density due to the small grain size in order to minimize the strain energy caused by grain boundaries [44,45]. It is assumed that smaller ferroelectric domains are responsible for the increased dielectric permittivity and ferroelectric remanent polarization ( $P_r$ ) and  $d_{33}$  [46,47].

The  $P$ - $E$  and  $I$ - $E$  hysteresis loops for the CNCBT ceramics measured at RT are presented in Fig. 6. While

the current peaks corresponding to the domain switching are observed in the  $I$ - $E$  loops (marked by the blue arrows) for the Na and Ce co-doped ceramics, pure CBT does not exhibit the ferroelectric switching up to a maximum  $E$  of 150 kV/cm. It is worth mentioning that the  $E$  of the current peak in  $I$ - $E$  loops does not exactly match with the field where the slope of polarization is the largest in  $P$ - $E$  loops. This inconsistency in the fields can be attributed to the presence of charged defects (e.g., oxygen vacancies) in



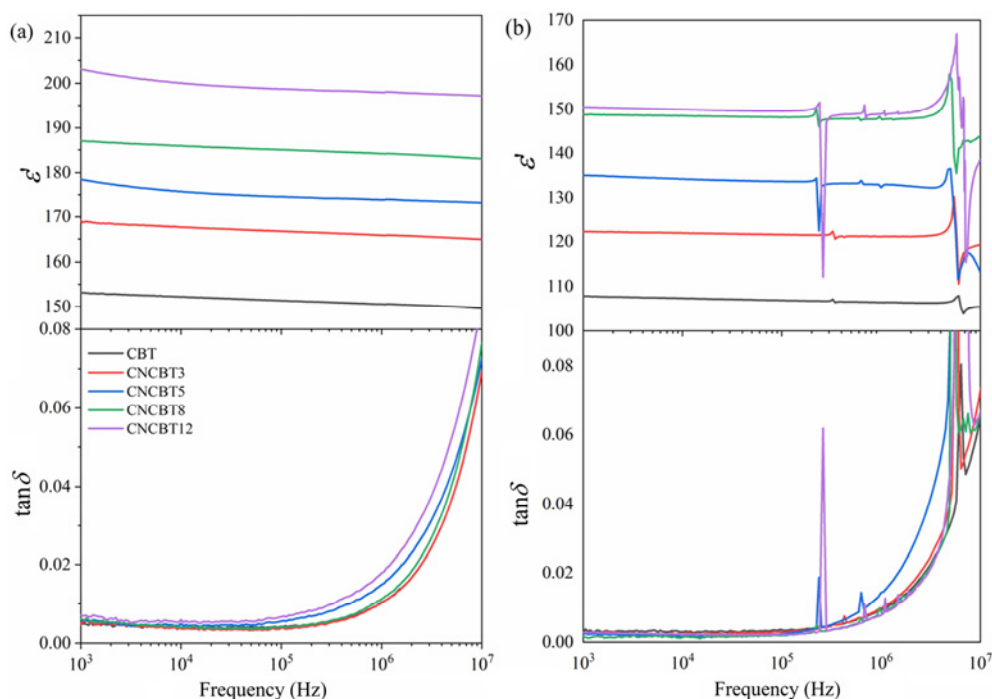
**Fig. 6**  $P$ - $E$  and  $I$ - $E$  hysteresis loops for (a) CBT, (b) CNCBT3, (c) CNCBT5, (d) CNCBT8, and (e) CNCBT12 ceramics, as recorded at RT (the current peaks are indicated by the blue arrows). (f)  $I$ - $E$  hysteresis loops for all CNCBT ceramics measured at 150 kV/cm and RT.

the ceramics [48,49]. Generally, in Aurivillius-phase ferroelectric ceramics, a high  $E$  needs to be applied to switch ferroelectric domains pinned by oxygen vacancies, which often causes dielectric breakdown of ceramics. For the CBT samples, the highest current at the maximum  $E$  is contributed by electrical conductivity. The  $E_c$ , at which the switching process occurs, decreases from 165 kV/cm in CNCBT3 to 135 kV/cm in CNCBT5, 120 kV/cm in CNCBT8, and 114 kV/cm in CNCBT12, which can be explained by the reduced domain size with higher domain wall mobility. Besides that, both the  $P_r$  and  $P_m$  increase on doping at RT ( $P_m = 9.8 \mu\text{C}/\text{cm}^2$  and  $P_r = 6.50 \mu\text{C}/\text{cm}^2$ ) for the CNCBT12 sample, which can be explained by the improved domain wall density and mobility, as reported in other ferroelectric ceramics [50,51]. Hence, it can be concluded that the introduction of  $\text{Na}^+$  and  $\text{Ce}^{3+/4+}$  ions into CBT is a viable method for the preparation of high-performance ferroelectric/piezoelectric materials for high-temperature applications.

Figures 7(a) and 7(b) show the frequency dependence of  $\epsilon'$  and  $\tan\delta$  for the unpoled and poled CNCBT ceramics, respectively. Upon doping, the permittivity increases due to the reduced oxygen vacancies and improved domain wall concentration and mobility. The permittivity of all the ceramic samples decreases slightly after DC poling, which can be explained by the

reduced density of non-180° domain walls and preferred domain growth [43,52]. The resonant peaks at high frequencies can be attributed to the piezoelectric effect. In addition, Table 1 summarizes the  $d_{33}$ ,  $K_p$ ,  $K_t$ , and  $Q_m$  for the poled CNCBT ceramics, as determined by the resonance–antiresonance method. The  $d_{33}$  increases from 5.5 pC/N (CBT) to 20.5 pC/N (CNCBT12), which can be linked with multi-sized domain structures. The normalized thermal depoling ( $d_{33}(T)/d_{33}(\text{RT})$ ) data for all CNCBT ceramics from RT to 700 °C are shown in Fig. S4 in the ESM. All values of  $d_{33}(T)/d_{33}(\text{RT})$  are over 0.9 when the annealing temperature is below or around 500 °C, suggesting good thermal stability of CNCBT12 piezoelectric ceramics. Similarly,  $K_t$  and  $K_p$  increase with the increasing content of Na and Ce, whereas  $Q_m$  shows the opposite trend. A high  $K_p$  value is usually related to higher  $d_{33}$ , which can be attributed to a high domain wall density. While the reduction of  $Q_m$  can be explained by the enhanced domain wall mobility accompanied by higher internal friction [53].

To further explore the relationship between the multiple-sized domain structure and ferroelectric/piezoelectric properties of CNCBT ceramics, the schematic diagrams are depicted in Figs. 8(a)–8(c). For a grain with various domains, as shown in Fig. 8(a), the double-well potential energy is deep, and the



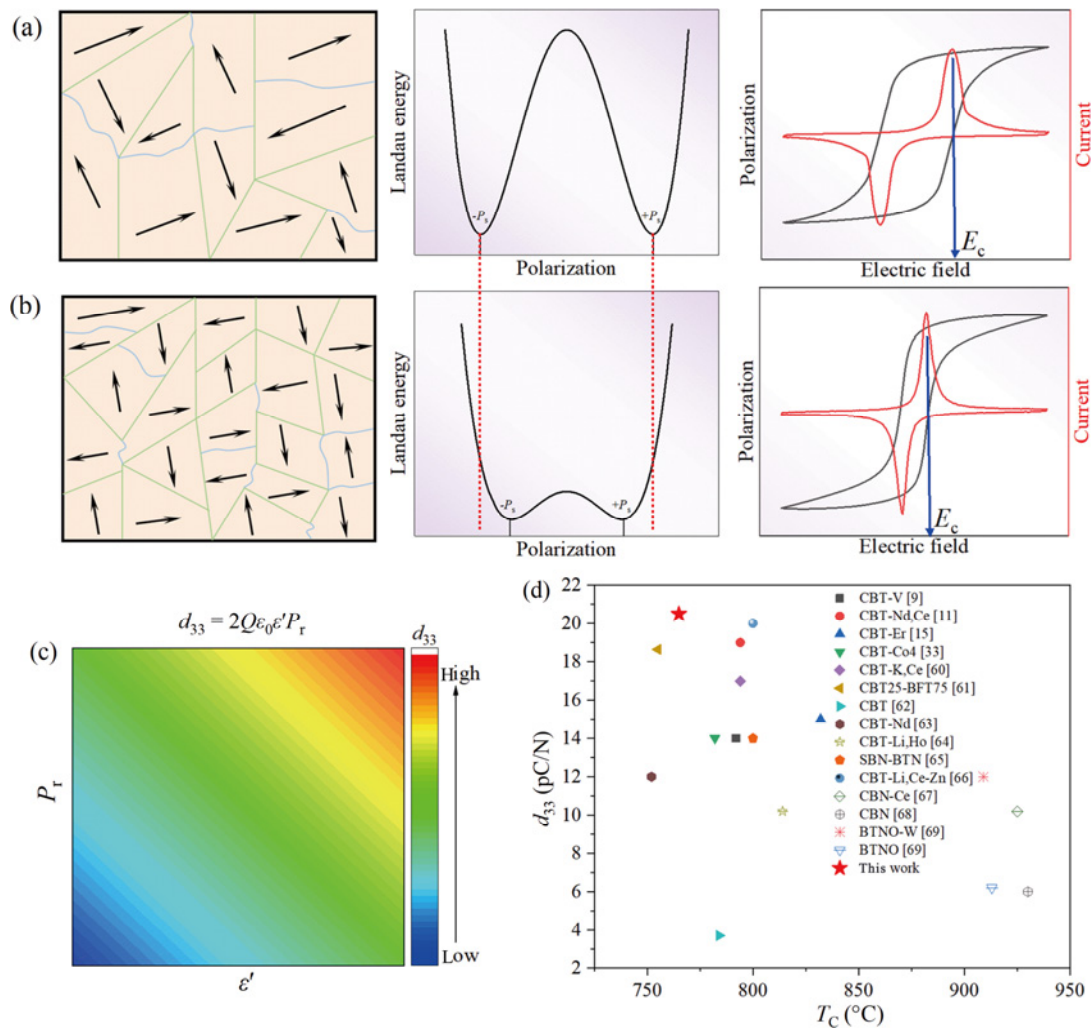
**Fig. 7**  $\epsilon'$  and  $\tan\delta$  as a function of frequency for (a) unpoled and (b) poled  $\text{Ca}_{1-x}(\text{Na}_{0.5}\text{Ce}_{0.5})_x\text{Bi}_4\text{Ti}_4\text{O}_{15}$  ceramics ( $x = 0, 0.03, 0.05, 0.08, \text{ and } 0.12$ ).

**Table 1**  $K_p$ ,  $K_i$ ,  $Q_m$ , and  $d_{33}$  for CNCBT ceramics, as obtained by the resonance–antiresonance method

| Composition | $K_p$ (%) | $K_i$ (%) | $Q_m$ | $d_{33}$ (pC/N) |
|-------------|-----------|-----------|-------|-----------------|
| CBT         | 3.3       | 12.5      | 4236  | 5.5±0.1         |
| CNCBT3      | 4.4       | 16.3      | 3290  | 10.5±0.1        |
| CNCBT5      | 5.3       | 17.8      | 2629  | 12.0±0.1        |
| CNCBT8      | 6.2       | 18.6      | 2298  | 15.3±0.1        |
| CNCBT12     | 7.3       | 19.7      | 700   | 20.5±0.1        |

saturated  $P$ – $E$  loop is broad with the two corresponding current peaks far away from  $E = 0$ . When the domains become smaller, as shown in Fig. 8(b), the double-well potential energy becomes flat accompanied by a reduced distance between two minimum points of  $-P_s$  and  $+P_s$  (negative and positive spontaneous polarization where the Landau energy is the lowest) indicated by

the red dashed lines. A slimmer  $P$ – $E$  loop with higher  $P_r$  and two current peaks with lower  $E_c$  (indicated by the blue arrows) can be observed. The relationship between  $d_{33}$  and electrostrictive coefficient ( $Q$ ) and dielectric and ferroelectric properties can be expressed by the equation of  $d_{33} = 2Q\epsilon_0\epsilon'P_r$  (where  $\epsilon_0$  is the permittivity of vacuum) [54], as shown in Fig. 8(c). For perovskite ferroelectrics, the product of  $Q$  and  $C$  is constant around  $(3.1 \pm 0.5) \times 10^3$  ( $\text{m}^4 \cdot \text{K})/\text{C}^2$  based on the thermodynamic analysis [55]. In this case,  $Q$  is proportional to  $C^{-1}$  for Aurivillius materials and decreases with  $x$  based on Fig. 4(f). Using a simple atomic model proposed by Newnham *et al.* [56,57], to the first approximation, the relationship between  $Q$  and dielectric properties can be written as  $Q \approx 1/\epsilon$ , where



**Fig. 8** Schematic diagrams of domain structures, potential energies, and hysteresis loops for (a) large-sized domains and (b) small-sized domains, where the blue curves indicate the 180° domain walls, and the green lines represent the non-180° domain walls. (c) Mapping of  $d_{33}$  at different values of  $P_m$  and  $\epsilon'$ . (d) Comparison between  $d_{33}$  and  $T_c$  values for  $x = 0.12$  sample and other Aurivillius piezoceramics reported in Refs. [9,11,15,33,60–69]. Note: BFT represents  $\text{Bi}_5\text{FeTi}_3\text{O}_{15}$ , SBN–BTN represents  $\text{SrBi}_2\text{Nb}_2\text{O}_9$ – $\text{Bi}_3\text{TiNbO}_9$ , and BTNO represents  $\text{Bi}_3\text{TiNbO}_9$ .

$\varepsilon$  is complex permittivity. Lower  $Q$  is related to higher dielectric permittivity, which suggest that an improved  $d_{33}$  is related to the increase of permittivity with higher  $x$  (Fig. 7). It is also reasonable that  $d_{33}$  is proportional to  $P_r$  here, which can be improved by the multi-sized domain configurations with a small backing field. A similar behaviour has been reported for other chemically modified Aurivillius materials [58]. Aside from these factors, reduced point defects like oxygen vacancies together with lower conductivity may destabilize domain structures, and then improve the domain wall mobility, thereby enhancing the piezoelectricity for CNCBT ceramics, as reported in other perovskite structured piezoelectric ceramics [59]. Overall, the enhanced  $d_{33}$  and a relatively high  $T_C$  for  $x = 0.12$  ceramics, as compared with those for other reported Aurivillius phase ceramics in Refs. [9,11,15, 33,60–69] (Fig. 8(d)), make the Na and Ce co-doped CBT ceramics promising materials for high-temperature piezoelectric applications.

#### 4 Conclusions

In summary, the effect of Na and Ce co-doping on the crystal structure, domain structure, and dielectric, ferroelectric, and piezoelectric properties of the Aurivillius-phase CBT-derived ceramics is investigated to prepare a high-performance piezoelectric material for high-temperature applications. The results of the XRD patterns on the  $\text{Ca}_{1-x}(\text{Na}_{0.5}\text{Ce}_{0.5})_x\text{Bi}_4\text{Ti}_4\text{O}_{15}$  ( $x = 0, 0.03, 0.05, 0.08, \text{ and } 0.12$ ) ceramics indicate that the crystal structure does not change substantially on doping, and all samples are single-phase materials with an orthorhombic structure (space group:  $A2_1am$ ), typical of the standard four-layer-structured BLSFs. The substitution-induced increase of  $t$  was found to result in the lowering ferroelectric-to-paraelectric phase transition temperature. The enhanced dielectric behaviour of the doped samples is attributed to the reduction of oxygen vacancies by the Na and Ce co-doping. By the PFM, the multi-sized (micron and sub-micron sized) ferroelectric domain structure was observed in the doped samples. It is demonstrated that the domain size progressively decreases with the increasing concentration of Na and Ce ions. The smaller domains with higher domain wall density and mobility are suggested to be responsible for the increased polarization, reduced  $E_c$ , and enhanced

piezoelectric properties of the CNCBT ceramics. The  $x = 0.12$  ceramic sample exhibiting a high  $T_C$  ( $\sim 765$  °C), large  $P_m$  ( $9.8 \mu\text{C}/\text{cm}^2$ ), and high  $d_{33}$  ( $20.5 \text{ pC}/\text{N}$ ) appears to be a promising candidate for high-temperature piezoelectric applications.

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#### Declaration of competing interest

The authors have no competing interests to declare that are relevant to the content of this article. The author Haixue Yan is the Editorial Committee member of this journal.

#### Electronic Supplementary Material

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